

THE TASK OF FREE VIBRATIONS OF HIGH-RISE BUILDINGS WITH A CYLINDRICAL RESERVOIR WITH FLUID

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Annotation: At the article theoretical investigates the problem of the transverse vibration of a high-rise structure carrying two concentrated masses using an integral transformation. The solutions of the frequency equation are obtained.

Keywords: Structure, concentrated masses, ground, frequency, Laplace-Carson transform.

MUJASSAMLASHGAN MASSALI INSHOOTNING KO'NDALANG TEBRANISHI MASALASI

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Annotatsiya: Maqolada mujassamlashgan ikki massali inshootning erkin ko'ndalang tebranishi masalasi integral almashtirish usuli yordamida nazariy tadqiq etilib, chastota tenglamasi yechilgan.

Kalit so'zlar: Inshoot, mujassamlashgan massa, grunt, chastota, Laplas-Karson almashtirishlari.

Tik inshootlarning tebranishini o'rganish muhandislik-qurilish sohalarida muhim amaliy ahamiyatga ega dolzarb masalalardan hisoblanadi. Odatda inshootga o'rnatilgan bitta mujassam massani inshoot bo'ylab shu massaga ekvivalent ikki yoki undan ortiq massa bilan almashtirish maqsadga muvofiq bo'ladi. Tashqi seysmik va garmonik kuchlar ta'sirida inshootning tebranma harakatini tahlil qilish, chastota va tebranish davrlarini aniqlash, inshootning turli qismlarida hosil bo'ladigan zo'riqishlar, kuchlanish va deformatsiyalarning tarqalishini, eguvchi moment, qiruvchi kuchlarni hisoblash yetarli qiyinchiliklarga ega bo'lib, qilingan ilmiy-nazariy ishda shu hisoblashlarni yengillashtirish, inshoot uchun murakkab tajribalar o'tkazilib olinadigan xarakterli kattaliklarni nazariy yo'l bilan olish mumkinligini ko'rsatish asosiy maqsad qilib olingan.

Ushbu maqolada o'zgaras ko'ndalang kesimli tik inshootning egilishidagi erkin va majburiy tebranma harakati masalasi tadqiq etilgan. Inshootning egilishi tebranma harakati asosidan turli masofalarda o'rnatilgan mujassamlashgan ikkita yuk bilan birgalikda tahlil etilgan. Mujassamlashgan yuklarni amalda mavjud, turli suyuqliklarga ega rezervuarlardan iborat jismlar deb ham qarash mumkin.

Tebranma harakat, garmonik tebranishlar va to'lqinlar, turli jismlar va sistemalarning va ularning birgalikdagi tabranma harakati masalalari, to'lqin harakati bilan bog'liq turli masalalar [1-4] adabiyotlarda atroflicha ko'rib chiqilgan.

Mujassamlashgan ikki massali yuk o'rnatilgan, o'zgaras ko'ndalang kesimli, tik inshootning erkin tebranma harakatini differensial tenglamasi

$$EJ \frac{\partial^4 u}{\partial x^4} = -m \frac{\partial^2 u}{\partial t^2} - M_1 \frac{\partial^2 u}{\partial t^2} \delta(x - l_1) - M_2 \frac{\partial^2 u}{\partial t^2} \delta(x - l_2) \quad (1)$$

ko'rinishda bo'ladi. Bu yerda M_1 hamda M_2 mos ravishda birinchi va ikkinchi yukning massasi [3].

(1) tenglama yechimini quyidagi

$$U(x, t) = \varphi(x) \cos \omega t \quad (2)$$

ko'rinishda izlaymiz.

Chegaraviy shartlar quyidagi ko'rinishda bo'lsin:

$$\begin{aligned} x=0: \quad U(0, t) = U'(0, t) = 0, \\ x=l: \quad -M_2 \frac{\partial^2 u}{\partial t^2} = EJ \frac{\partial^3 u}{\partial x^3}, \quad EJ \frac{\partial^2 u}{\partial x^2} = 0. \end{aligned} \quad (3)$$

(2) dan mos hosilalarni olib, (1) ga qo'ysak:

$$\varphi^{IV}(x) - \frac{m\omega^2}{EJ} \varphi(x) = \frac{M_1}{EJ} \omega^2 \varphi(l_1) \delta(x-l_1) + \frac{M_2}{EJ} \omega^2 \varphi(l_2) \delta(x-l_2) \quad (4)$$

kelib chiqadi.

Qulaylik uchun quyidagi belgilashlarni kiritamiz:

$$k^4 = \frac{m\omega^2}{EJ}; Q_1 = \frac{M_1}{EJ} \omega^2; Q_2 = \frac{M_2}{EJ} \omega^2;$$

Natijada (4) tenglama quyidagi ko'rinishga keladi:

$$\varphi^{IV}(x) - k^4 \varphi(x) = Q_1 \varphi(l_1) \delta(x-l_1) + Q_2 \varphi(l_2) \delta(x-l_2). \quad (5)$$

$\varphi(x)$ ga mos chegaraviy shartlar esa quyidagicha bo'ladi:

$$\begin{aligned} x=0: \quad \varphi(0) &= 0, \\ \varphi'(0) &= 0, \\ x=l: \quad M_2 \omega^2 \varphi(l) &= EJ \varphi'''(l), \\ \varphi''(l) &= 0. \end{aligned} \quad (6)$$

Laplas-Karson integral almashtirishlari yordamida (5) ni integrallaymiz. Yechimni aniqlashda (5) tenglamani har bir hadini e^{-px} ga ko'paytirib, 0 dan ∞ gacha integrallaymiz:

$$\Phi(p) \xrightarrow{\cdot} \varphi(x) \quad \Phi(p) = p \int_0^{\infty} \varphi(x) e^{-px} dx, \quad (7)$$

$$F(p) \rightarrow f(x) = Q_1 \varphi(l_1) \delta(x-l_1) + Q_2 \varphi(l_2) \delta(x-l_2), \quad (8)$$

$$p \int_0^{\infty} \varphi^{IV}(x) e^{-px} dx = -p \varphi'''(0) - p^2 \varphi''(0) - p^3 \varphi'(0) - p^4 \varphi(0) + p^4 \Phi(p), \quad (9)$$

$$k^4 p \int_0^{\infty} \varphi(x) e^{-px} dx = k^4 \Phi(p), \quad (10)$$

$$\begin{aligned} p \int_0^{\infty} f(x) e^{-px} dx &= p \int_0^{\infty} [Q_1 \varphi(l_1) \delta(x-l_1) + Q_2 \varphi(l_2) \delta(x-l_2)] e^{-px} dx = \\ &= p Q_1 \varphi(l_1) e^{-pl_1} + p Q_2 \varphi(l_2) e^{-pl_2}. \end{aligned} \quad (11)$$

Chegaraviy shartlardan foydalanib, $\Phi(p)$ ni topamiz:

$$\begin{aligned} \Phi(p) [p^4 - k^4] - p \varphi'''(0) - p^2 \varphi''(0) &= p [Q_1 \varphi(l_1) e^{-pl_1} + Q_2 \varphi(l_2) e^{-pl_2}], \\ \Phi(p) - \frac{p}{p^4 - k^4} \varphi'''(0) - \frac{p^2}{p^4 - k^4} \varphi''(0) &= \frac{p}{p^4 - k^4} [Q_1 \varphi(l_1) e^{-pl_1} + Q_2 \varphi(l_2) e^{-pl_2}]. \end{aligned}$$

Funksiyalardan “asli”ga qaytish uchun Laplas-Karson almashtirishlaridan foydalanamiz:

$$\begin{aligned} \frac{p}{p^4 - k^4} \varphi'''(0) &= \frac{1}{k^3} V(kx) \varphi'''(0), \quad \frac{p}{p^4 - k^4} \varphi''(0) = \frac{1}{k^2} U(kx) \varphi''(0), \\ \frac{p}{p^4 - k^4} Q_1 \varphi(l_1) e^{-pl_1} &= \frac{1}{k^3} V(k(x-l_1)) Q_1 \varphi(l_1), \quad \frac{p}{p^4 - k^4} Q_2 \varphi(l_2) e^{-pl_2} = \frac{1}{k^3} V(k(x-l_2)) Q_2 \varphi(l_2). \end{aligned} \quad (12)$$

Demak,

$$\begin{aligned} \Phi(p) \xrightarrow{\cdot} \varphi(x) &= \frac{1}{k^3} V(kx) \varphi'''(0) + \frac{1}{k^2} U(kx) \varphi''(0) + \\ &+ \frac{Q_1 \varphi(l_1)}{k^3} V(k(x-l_1)) \theta(x-l_1) + \frac{Q_2 \varphi(l_2)}{k^3} V(k(x-l_2)) \theta(x-l_2). \end{aligned} \quad (13)$$

Qulaylik uchun quyidagicha belgilashlar kiritamiz:

$$\begin{aligned} A &= \frac{Q_1 Q_2 V(k(l_1-l_2)) U(kl_2) + k^3 Q_1 U(kl_1)}{k^8 + k^2 Q_1 Q_2 V^2(k(l_2-l_1))}, \quad B = \frac{Q_2 Q_1 V(k(l_2-l_1)) U(kl_1) + k^3 Q_2 U(kl_2)}{k^8 + k^2 Q_1 Q_2 V^2(k(l_2-l_1))}, \\ C &= \frac{Q_1 Q_2 V(k(l_1-l_2)) V(kl_2) + k^3 Q_1 U(kl_1)}{k^9 + k^3 Q_1 Q_2 V^2(k(l_2-l_1))}, \quad D = \frac{Q_1 Q_2 V(k(l_2-l_1)) V(kl_1) + k^3 Q_2 U(kl_2)}{k^9 + k^3 Q_1 Q_2 V^2(k(l_2-l_1))}, \end{aligned} \quad (14)$$

$$E = S(kl) + Ak^2 T(k(l-l_1)) + Bk^2 T(k(l-l_2)), \quad F = \frac{1}{k} T(kl) + Ck^2 T(k(l-l_1)) + Dk^2 T(k(l-l_2)), \quad (15)$$

$$G = kV(kl) + Ak^3 S(k(l-l_1)) + Bk^3 S(k(l-l_2)), \quad H = S(kl) + Ck^3 S(k(l-l_1)) + Dk^3 S(k(l-l_2)),$$

bu yerda $S(x)$, $T(x)$, $U(x)$, $V(x)$ funksiyalar Krilov funksiyalari.

Demak, biz izlayotgan yechim quyidagi ko‘rinishda bo‘lishi aniqlanadi:

$$\begin{aligned} \varphi(x) = & \left(\frac{1}{k^2} U(kx) + AV(k(x-l_1))\theta(x-l_1) + BV(k(x-l_2))\theta(x-l_2) \right) \varphi''(0) + \\ & + \left(\frac{1}{k^3} V(kx) + CV(k(x-l_1))\theta(x-l_1) + DV(k(x-l_2))\theta(x-l_2) \right) \varphi'''(0). \end{aligned} \quad (16)$$

Endi chegaraviy shartlardan foydalanib, umumiy yechimni aniqlaymiz. Ma'lumki, $\varphi''(0)$, $\varphi'''(0)$ yagona yechimga ega bo'lishi uchun ular oldidagi koeffitsiyentlardan tuzilgan determinant 0 ga teng bo'lishi kerak:

$$\begin{cases} (S(kl) + Ak^2T(k(l-l_1)) + Bk^2T(k(l-l_2)))\varphi''(0) + \\ + \left(\frac{1}{k} T(kl) + Ck^2T(k(l-l_1)) + Dk^2T(k(l-l_2)) \right) \varphi'''(0) = 0 \\ (kV(kl) + Ak^2S(k(l-l_1)) + Bk^3S(k(l-l_2)))\varphi''(0) + \\ + (S(kl) + Ck^3S(k(l-l_1)) + Dk^3S(k(l-l_2)))\varphi'''(0) = 0 \end{cases} \quad (17)$$

(17) tenglamalardan $k_1, k_2, k_3, \dots, k_n$ lar aniqlanadi va mos $\omega_1, \omega_2, \omega_3, \dots, \omega_n$ chastotalar bir qiymatli aniqlanadi, so'ngra $T_i = \frac{2\pi}{\omega_i}$ ifodadan har bir chastotaga mos tebranish davrlari topiladi. Elektron hisoblash

mashinasida *Maple 13* matematik dasturiy paketi yordamida aniqlangan k_i larning qiymatlari quyida jadvalda keltirilgan. Jadvalda keltirilgan chastota tenglamasining ildizlari inshoot va mujassamlashgan yuklarning o'rnatilish masofalari va massalarining turli qiymatlari uchun olingan.

Ushbu belgilashlarni kiritamiz:

$$Q_1 = \frac{M_1 \omega}{EJ} = \frac{M_1 E J k^4}{m E J} = \frac{M_1}{m} k^4, \quad k^4 = Q_1 \frac{M_1}{m}, \quad k = \sqrt[4]{Q_1 \frac{M_1}{m}}, \quad \omega = \sqrt{\frac{EJ}{m}} k^4. \quad (17)$$

Chastota tenglamalarining aniqlangan ildizlari jadvali

		k_i		k_i		k_i		k_i
l, m	40	0,0468	50	0,0374	100	0,0469	100	0,0469
l_1, m	30	0,1963	25	0,1570	20	0,1413	20	0,1413
l_2, m	20	0,2748	50	0,2826	70	0,2356	50	0,2357
M_1, kg	$2 \cdot 10^3$	0,3534	$4 \cdot 10^3$	0,3435	$1,1 \cdot 10^3$	0,3534	$1,1 \cdot 10^3$	0,3298
M_2, kg	10^3	0,4319	$2 \cdot 10^3$	0,4082	$3 \cdot 10^3$	0,4082	$3 \cdot 10^3$	0,4555
Q_1	$0,02k^4$	0,5104	$0,04k^4$	0,5340	$0,04k^4$	0,5340	$0,04k^4$	0,5774
Q_2	$0,01k^4$	0,6675	$0,02k^4$	0,6597	$0,02k^4$	0,6597	$0,02k^4$	0,6544

Shunday qilib, birinchi holda, ikki mujassamlangan massali yuk o'rnatilgan tik gidroinshootning sof egilishidagi erkin tebranma harakati differensial tenglamasi, mos chegaraviy shartlarda olinib, shu inshootning xususiy tebranish chastota va davrlari topildi, umumiy yechim Laplas-Karson integral almashtirishlari yordamida aniqlandi. Har bir ko'ndalang kesimlarda hosil bo'ladigan eguvchi moment va qirquvchi kuch qiymatlarini aniqlovchi ifodalar aniqlandi. Ikkinchi holda aynan shu inshootning asosi tashqi qo'zg'atuvchi garmonik kuch ta'siri bilan harakatda bo'lgandagi majburiy tebranma harakati tahlil etildi. Gidroinshootning erkin va majburiy tebranma harakatini xarakterlaydigan asosiy kattaliklarning o'zgarish qonunlari olinib, tahlil qilindi.

Bajarilgan ushbu ilmiy tadqiqot ishi natijalaridan uning mavzusiga yaqin ilmiy, ilmiy-amaliy, tajribaviy ishlarni bajarishda, xususan, mujassamlashgan massali tik gidroinshootlarning murakkab fazoviy tebranishlarini tadqiq etishda nazariy qo'llanma sifatida foydalanish mumkin.

Adabiyotlar

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